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characteristics other than thermal characteristics, such as particle size distribution, degree of spherical shape and the like, are comparable to the characteristics of current silica fillers, there is a possibility that the thermal characteristics, viscosity and moldability can be simultaneously improved to an unprecedented extent. From this standpoint, attempts to replace "some part" of silica with an aluminum nitride powder have been published (for example, see Japanese Patent Application Laid-Open No. 9-183610/1997). At the current point in time, however, aluminum nitride powders which have the particle size (several microns to several tens of microns) required in a filler powder are manufactured mainly by the direct nitridation process, in which manufacture is accomplished by a pulverization process. Accordingly, such powders are non-spherical powders which have angular shapes, and therefore suffer from the drawback of a conspicuously lowered viscosity and moldability. The direct-nitridation is conventionally a batch type production, so that the productivity is very low. Accordingly, the simultaneous addition of a spherical silica powder is considered necessary, and the only method of use that has been possible is a method in which only a portion of the silica is replaced.--

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Please delete the paragraph beginning at page 4, line 9, and replace with the following.

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--The reduction nitridation (carbothermal-reaction) method in which a mixture of alumina and carbon is sintered in a nitrogen atmosphere also exists as an industrial manufacturing method alongside the direct nitridation method. In the case of the reduction nitridation method, in which no pulverization process is necessary, a powder with a relatively high degree of spherical shape can be manufactured. However, current reduction nitridation processes have been established mainly as processes for supplying the raw-material powders

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of sinters. Accordingly, such processes deal mainly with powders whose mean particle size is on the sub-micron order, and have not been devised so that powders that have a particle size on the order of ten-odd microns or greater, which are mainly required as filler powders, can easily be used. Furthermore, in the case of the reduction nitridation method which involves an endothermic reaction that is the exact opposite of the exothermic direct nitridation method, a heat treatment for a fixed time or longer in the high-temperature region of approximately 1500 to 1800°C is essential, and in cases where a raw-material powder of alumina or the like with a large particle size is prepared in order to manufacture a powder with a relatively large particle size such as a filler powder, it has not been confirmed that a reduction nitridation process can be proceeded efficiently by using an electric furnace alone. --

Please insert the following paragraph after page 5, line 7.

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--Another conventional method of the carbothermal-reaction is to use simultaneously a reacting-agent in order to lower the temperature of endothermic reaction, and to produce a larger sized crystal. For example, an unagglomerated single crystal having a size of around 10  $\mu\text{m}$  have been published through the carbothermal-reaction with using simultaneously a reacting-agent such as alkali metals, preferably  $\text{Na}_2\text{O}$  (for example, see USA Patent No. 5190738/1993). The powder would be improved the remained oxygen content and sufficient for reinforcement as a mechanical application; but not for LSI. The powder contains inherently the added alkali metal and derives a crucial lattice defect, which degrades the thermal conductivity. The remained alkali, especially soda (Na) element, is highly troublesome and hateful element for reacting easily to a constituent of LSI such as silicon. Besides, the carbothermal-reactions are conventionally batch type production, so that the productivity is very low.--